

Volumetric Properties of 3-Methylbutyl Ethanoate with Ethyl Acrylate, Butyl Acrylate, Methyl Methacrylate, and Styrene at 25°C

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Densities of the binary systems of 3-methylbutyl ethanoate (*isoamyl acetate*) with ethyl acrylate, butyl acrylate, methyl methacrylate, and styrene have been measured as a function of composition at 25°C and atmospheric pressure using an Anton Paar DMA 5000 oscillating U-tube densimeter. The calculated excess volumes were correlated with the Redlich–Kister equation and with a series of Legendre polynomials. The excess volumes are positive for the binary systems of 3-methylbutyl ethanoate with each of the three acrylate monomers and negative for the system with styrene. The 3-methylbutyl ethanoate + butyl acrylate system exhibits near-ideal behavior.

KEY WORDS: acrylates; densities; 3-methylbutyl ethanoate; excess volumes; monomers; styrene.

1. INTRODUCTION

The mixing of different compounds gives rise to solutions that generally do not behave ideally. The deviation from ideality may be expressed by many thermodynamic variables, particularly by excess properties. Excess thermodynamic properties of mixtures correspond to the difference between the actual property and the property if the system behaves ideally, and thus are useful in the study of molecular interactions and arrangements. In particular, they reflect the interactions that take place between solute–solute, solute–solvent, and solvent–solvent species. Excess volumes represent the first derivative of the excess Gibbs function with respect to the

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pressure, $V^E = (\partial G^E / \partial P)_{T,n}$, and the pertinent partial excess volume corresponds to the variation of the chemical potential with pressure, $\bar{V}_i^E = (\partial \mu_i / \partial P)_{T,n}$.

This work is part of our program to provide data for the characterization of the molecular interactions between solvents and commercially important monomers, in particular the influence of the chemical structure of the solute in the systems under consideration. So far we have studied the volumetric behavior of the monomers with cyclic hydrocarbons [1], aromatic solvents [2–4] and aliphatic and cyclic ethers [5–7]. 3-Methylbutyl ethanoate (banana oil) is an excellent solvent and may be useful in polymerization and other chemical reactions such as hydrogenation, in the cleaning of polymer surfaces, electronic materials, etc. Acrylic esters and styrene are important industrial chemicals used in the large-scale preparation of useful polymers. The esters are also interesting because they contain both a double bond and an ester group.

To the best of our knowledge no literature data are available for the excess volumes of the systems of 3-methylbutyl ethanoate with ethyl acrylate, butyl acrylate, methyl methacrylate, and styrene.

2. EXPERIMENTAL

2.1. Materials

3-Methylbutyl ethanoate, (*isoamyl acetate*, 99.34 mass%), ethyl acrylate, EA, (99.8 mass%), butyl acrylate, BA, (99.9 mass%), methyl methacrylate, MMA, (99.9 mass%), and styrene (99.9 mass%) were purchased from Aldrich. The supplier certified the purity of all the reagents by gas chromatography analysis. EA, BA, and MMA were vacuum distilled prior to use to eliminate the stabilizer (about 0.002% mass of hydroquinone monomethyl ether). Styrene, containing 10–15 ppm of 4-*tert*-butylcatechol as stabilizer, was not distilled to avoid polymerization but was degassed by freezing and heating. After purification, all reagents were stored under molecular sieves. The purity of the solvents was further substantiated by comparing their densities at 25°C with values reported in the literature (Table I).

2.2. Density Measurements

The density of the samples was measured with an Anton Paar model DMA 5000 oscillating U-tube densimeter, provided with automatic viscosity correction, two integrated Pt 100 platinum thermometers (DKD traceable), and with a stated uncertainty of $5 \times 10^{-6} \text{g}\cdot\text{cm}^{-3}$. The temperature

Table I. Purities and Densities of Pure Components at 25°C

Component	Purity (mass%)	Density (g·cm ⁻³)	
		Meas.	Lit.
3-Methyl butyl ethanoate (1)	99.34	0.867356	0.86843[13]
Butyl acrylate (2)	99.9	0.893947	0.8941[14]
Ethyl acrylate (3)	99.8	0.916124	0.9163[14]
Methyl methacrylate (4)	99.9	0.937628	0.93766[15]
Styrene (5)	99.9	0.901941	0.9016 [16]

in the cell was regulated to ± 0.001 K with a solid-state thermostat. The apparatus was calibrated daily with dry air and bi-distilled freshly degassed water.

All liquids were boiled or heated to remove dissolved air. Solutions of different compositions were prepared by mass in a 10 cm³ rubber-stoppered vial to prevent evaporation, using a Mettler AG balance accurate to $\pm 10^{-4}$ g. To minimize the errors in composition, the heavier component was charged first and the sample kept in ice water. The total uncertainty (ISO 9001) in the mole fraction is 7.98×10^{-5} ; the precision of the density (duplicate) measurements is $\pm 2 \times 10^{-6}$ g·cm⁻³, and that of the temperature is ± 0.002 K. The total uncertainty in the density measurement, as reported by the equipment manufacturer, is 5×10^{-6} g·cm⁻³ and includes the calibration procedure.

Proper safety measures were taken when handling all the materials.

3. RESULTS AND DISCUSSION

At least 21 density measurements were performed (with repetition) for each binary system over the full concentration range ($0 \leq x \leq 1$). The excess volumes V^E of the solutions of molar composition x were calculated from the densities of the pure liquids and their mixtures according to the following equation:

$$V^E = [xM_1 + (1-x)M_2]/\rho - [xM_1/\rho_1 + (1-x)M_2/\rho_2] \quad (1)$$

where ρ , ρ_1 , and ρ_2 are the densities of the solution and pure components 1 and 2, respectively, and M_1 and M_2 are the molar masses of the pure components. The corresponding values of ρ and V^E are reported in Tables II to V and Fig. 1.

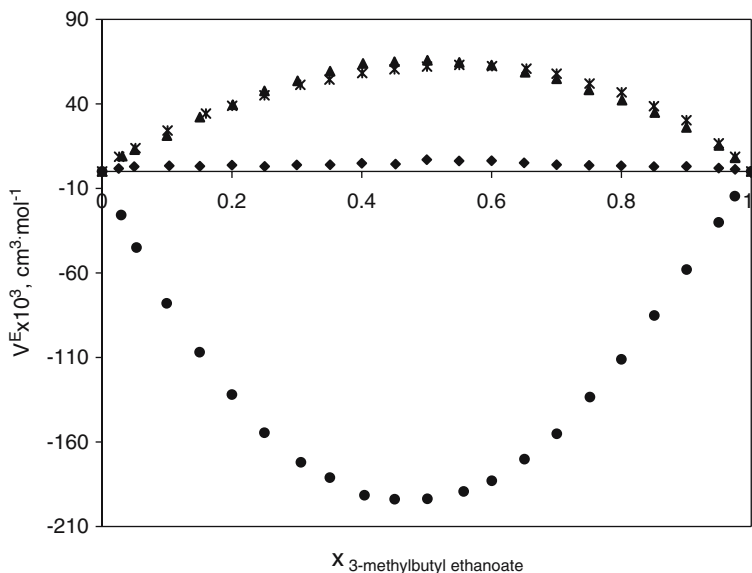


Fig. 1. Excess volumes at 298.15 K: *3-methylbutyl ethanoate + MMA; ▲3-methylbutyl ethanoate + EA; ◆ 3-methylbutyl ethanoate + BA; ● 3-methylbutyl ethanoate + styrene.

The first term in Eq. (1) represents the actual volume of the solution, and the second, the volume it would occupy if the mixture behaved ideally. In general, while these two volumes are similar in size (usually larger than $100 \text{ cm}^3 \cdot \text{mol}^{-1}$), their difference is usually smaller by two to three orders of magnitude and thus carries a significantly larger error.

Partial molar volumes were calculated using the relations [8],

$$\bar{V}_1 = V + x_2 \frac{dV}{dx_1} \quad (2)$$

$$\bar{V}_2 = V - x_1 \frac{dV}{dx_1} \quad (3)$$

The pertinent values are reported in Table VI and are necessarily consistent.

The values of V^E were correlated with composition using two methods.

(a) The Redlich–Kister expression [9],

$$V^E = x_1 x_2 \sum_{k=0}^n A_k (x_1 - x_2)^k \quad (4)$$

Table II. Experimental Densities, Molar Volumes, Calculated Excess Volumes, and Deviations δV^E ($\delta V^E = V_{\text{expt}}^E - V_{\text{calc}}^E$) for the 3-Methylbutyl Ethanoate (1) + Butyl Acrylate (2) System at 25°C

x_1	$\rho(\text{g}\cdot\text{cm}^3)$	V ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 \delta V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)
0	0.893947	143.3754	0	0
0.0257	0.893222	143.5498	1.7980	-0.07
0.0496	0.892552	143.7117	2.8609	-0.01
0.1035	0.891059	144.0747	3.4107	-0.2
0.1504	0.889769	144.3902	3.1018	-0.3
0.2000	0.888407	144.7243	3.7951	0.7
0.2504	0.887040	145.0619	2.9886	-0.2
0.2999	0.885689	145.3963	3.9056	0.4
0.3512	0.884304	145.7411	4.0588	-0.2
0.4001	0.882985	146.0706	4.8667	-0.1
0.4521	0.881596	146.4200	4.3701	-1
0.5000	0.880304	146.7448	7.0043	1
0.5500	0.878984	147.0800	6.2586	0.2
0.6000	0.877664	147.4163	6.3475	0.5
0.6500	0.876356	147.7517	5.1423	-0.07
0.7003	0.875048	148.0886	4.0557	-0.4
0.7502	0.873751	148.4238	3.6748	-0.1
0.7998	0.872467	148.7571	3.3661	0.07
0.8500	0.871176	149.0938	2.8609	-0.1
0.9000	0.869889	149.4306	3.0344	0.3
0.9500	0.868618	149.7654	1.9960	-0.04
0.9752	0.867980	149.9342	1.2457	-0.01
1	0.867356	150.0998	0	0

where the A_k 's are the adjustable parameters of the model. The Redlich-Kister equation was originally developed to correlate the excess Gibbs function and calculate the values of activity coefficients. It turned out to be such a powerful and versatile correlating tool that its use has been extended to other properties, particularly, excess volumes and excess enthalpies of mixing. Nevertheless, it suffers from the important drawback that the values of its adjustable parameters change as the number of terms in the series is increased, so that no physical interpretation can be attached to them.

(b) A series of Legendre polynomials $L_k(x_1)$,

$$V^E = x_1 x_2 \sum_{k=0}^n a_k L_k(x_1) \quad (5)$$

Table III. Experimental Densities, Molar Volumes, Calculated Excess Volumes, and Deviations δV^E ($\delta V^E = V_{\text{expt}}^E - V_{\text{calc}}^E$) for the 3-Methylbutyl Ethanoate (1) + Ethyl Acrylate (3) System at 25°C

x_1	$\rho(\text{g}\cdot\text{cm}^3)$	V ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 \delta V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)
0	0.916124	109.2865	0	0
0.0310	0.913999	110.5591	9.0815	1
0.0501	0.912721	111.3458	12.982	0.6
0.0999	0.909503	113.3850	21.227	-1
0.1505	0.906326	115.4620	32.155	0.4
0.2012	0.903286	117.5372	39.544	-0.5
0.2501	0.900442	119.5430	47.669	0.4
0.3010	0.897604	121.6253	53.588	-0.3
0.3512	0.894897	123.6805	59.359	0.2
0.4020	0.892257	125.7586	63.971	0.8
0.4505	0.889840	127.7396	64.963	-0.4
0.5010	0.887406	129.7993	65.849	-0.2
0.5502	0.885117	131.8082	64.610	-0.5
0.6002	0.882870	133.8436	62.978	0.3
0.6518	0.880634	135.9458	58.693	-0.2
0.7001	0.878602	137.9132	54.887	0.7
0.7499	0.876582	139.9402	48.348	-0.3
0.8008	0.874573	142.0131	42.223	0.06
0.8514	0.872644	144.0689	34.915	0.1
0.9001	0.870846	146.0495	26.073	-0.3
0.9503	0.869055	148.0862	15.408	0.2
0.9752	0.868197	149.0941	8.0672	-0.2
1.0000	0.867356	150.0998	0	0

which for the four first terms ($k = 0, 1, 2, 3$) becomes

$$V^E = x_1 x_2 [a_0 + a_1(2x_1 - 1) + a_2(6x_1^2 - 6x_1 + 1) + a_3(20x_1^3 - 30x_1^2 + 12x_1 - 1)] \quad (6)$$

Legendre polynomials belong to the category of orthogonal functions such as Fourier, Bessel, and Chebyshev, which have the valuable characteristic that for a continuous series of observations (infinite), the values of the coefficients do not change as the number of terms in the series is increased. This is an important property because if a physical interpretation can be assigned to one of the coefficients, its value remains constant. For the case of discrete measurements, such as determination of volumes of mixing, the values of the coefficients will vary, but only slightly. In addition, it can be shown that the series of Legendre polynomials have the important characteristic that the structure of its first four terms is

Table IV. Experimental Densities, Molar Volumes, Calculated Excess Volumes, and Deviations δV^E ($\delta V^E = V_{\text{expt}}^E - V_{\text{calc}}^E$) for the 3-Methylbutyl Ethanoate (1) + Methyl Methacrylate (3) System at 25°C

x_1	$\rho(\text{g}\cdot\text{cm}^3)$	V ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 \delta V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)
0	0.937628	106.7801	0	0
0.0263	0.934984	107.9270	8.7730	0.9
0.0515	0.932526	109.0251	13.848	-0.4
0.1007	0.927871	111.1658	24.184	-0.3
0.1599	0.922520	113.7398	34.245	0.3
0.2002	0.919025	115.4930	38.933	-0.4
0.2500	0.914860	117.6532	45.038	-0.05
0.3053	0.910408	120.0550	51.323	0.7
0.3502	0.906930	122.0072	54.399	-0.2
0.4005	0.903170	124.1889	58.299	0.1
0.4504	0.899578	126.3530	60.478	-0.4
0.5005	0.896102	128.5221	62.088	-0.4
0.5502	0.892767	130.6765	63.107	0.1
0.6005	0.889513	132.8559	62.282	-0.06
0.6538	0.886188	135.1613	60.822	0.6
0.7003	0.883384	137.1751	57.807	0.5
0.7508	0.880451	139.3563	51.983	-0.7
0.8003	0.877660	141.4951	46.823	-0.02
0.8500	0.874956	143.6425	38.641	-0.6
0.9002	0.872311	145.8074	30.313	0.9
0.9499	0.869798	147.9472	16.689	-0.1
0.9751	0.868558	149.0308	8.7091	-0.2
1	0.867356	150.0998	0	0

the same as that of the first four terms of the Redlich–Kister expression. Tomiska [10, 11] has described the mathematical procedure to transform a power expansion, such as that of Redlich–Kister, into an orthogonal series. In addition, Tomiska has provided the iteration formulas for Legendre or Chebyshev series of any order as well as the proof that the procedure is independent of the conversion coefficients from the actual excess property.

Equations (4) and (5) were fitted using a least-squares optimization procedure, with all points weighted equally and minimizing the following objective function (OF):

$$\text{OF} = \sum_1^N (V_{i,\text{expt}}^E - V_{i,\text{calc}}^E)^2, \quad (7)$$

Table V. Experimental Densities, Molar Volumes, Calculated Excess Volumes, and Deviations δV^E ($\delta V^E = V_{\text{expt}}^E - V_{\text{calc}}^E$) for the 3-Methylbutyl Ethanoate (1) + Styrene (5) System at 25°C

x_1	$\rho(\text{g}\cdot\text{cm}^3)$	V ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)	$10^3 \delta V^E$ ($\text{cm}^3\cdot\text{mol}^{-1}$)
0	0.901941	115.473	0	0
0.0293	0.900833	116.463	-25.761	-0.2
0.0529	0.899946	117.260	-45.044	-0.7
0.0997	0.898180	118.846	-78.029	-0.5
0.1502	0.896274	120.567	-106.88	1
0.2000	0.894422	122.267	-131.90	1
0.2502	0.892590	123.982	-154.58	-1
0.3064	0.890541	125.910	-172.01	-0.6
0.3509	0.888929	127.443	-181.05	1
0.4042	0.887046	129.278	-191.52	-1
0.4508	0.885398	130.888	-193.81	0.4
0.5011	0.883646	132.629	-193.59	0.7
0.5571	0.881719	134.575	-189.32	0.1
0.6002	0.880257	136.072	-182.94	-0.6
0.6507	0.878546	137.836	-170.13	-0.03
0.7003	0.876895	139.568	-155.21	-1
0.7514	0.875198	141.358	-133.45	0.7
0.7999	0.873614	143.061	-111.05	0.7
0.8507	0.871983	144.845	-85.237	0.3
0.9005	0.870410	146.597	-58.076	-0.3
0.9499	0.868881	148.334	-30.045	-1
0.9747	0.868119	149.208	-14.568	0.06
1	0.867356	150.100	0	0

where N is the number of observations. The values of the different adjustable parameters, A_k and a_k , are reported in Tables VII and VIII for different values of k , together with the pertinent statistics. The standard deviation s was calculated as

$$s = \left[\sum (V_{i,\text{expt}}^E - V_{i,\text{calc}}^E)^2 / (N - k) \right]^{1/2}, \quad (8)$$

where k is the number of adjustable parameters. The statistical significance of adding one or more terms after the third was examined using a χ^2 -based test, coupled to the requirement that the residues be randomly distributed, as suggested by Wisniak and Polishuk [12]. It was not deemed necessary to perform a step-wise regression.

A plot of the function $V^E/x_i x_j$ against composition was used in every case to test the quality of the data; this function is extremely sensitive

Table VI. Partial Molar Volumes \bar{V}_i , in $\text{cm}^3 \cdot \text{mol}^{-1}$

x_1	3-Methylbutyl ethanoate (1)+ BA (2)		3-Methylbutyl ethanoate (1)+ EA (3)		3-Methylbutyl ethanoate (1)+ MMA (4)		3-Methylbutyl ethanoate (1)+ St (5)	
	\bar{V}_2	\bar{V}_1	\bar{V}_3	\bar{V}_1	\bar{V}_4	\bar{V}_1	\bar{V}_5	\bar{V}_1
0	143.375	150.192	109.287	150.376	106.780	150.425	115.473	149.187
0.05	143.377	150.131	109.288	150.323	106.782	150.340	115.470	149.322
0.10	143.379	150.105	109.290	150.295	106.786	150.289	115.461	149.433
0.15	143.381	150.099	109.294	150.279	106.792	150.259	115.448	149.525
0.20	143.383	150.104	109.300	150.269	106.798	150.242	115.431	149.603
0.25	143.386	150.115	109.309	150.262	106.805	150.234	115.412	149.671
0.30	143.392	150.128	109.324	150.257	106.815	150.230	115.389	149.731
0.35	143.402	150.142	109.346	150.252	106.829	150.229	115.362	149.786
0.40	143.416	150.156	109.374	150.250	106.847	150.229	115.332	149.836
0.45	143.434	150.170	109.407	150.251	106.868	150.232	115.298	149.882
0.50	143.455	150.184	109.444	150.255	106.893	150.235	115.260	149.925
0.55	143.476	150.198	109.481	150.260	106.919	150.237	115.217	149.963
0.60	143.494	150.209	109.514	150.265	106.944	150.239	115.170	149.998
0.65	143.506	150.217	109.540	150.267	106.967	150.237	115.121	150.028
0.70	143.509	150.219	109.555	150.264	106.987	150.230	115.069	150.053
0.75	143.501	150.213	109.558	150.251	107.001	150.217	115.018	150.072
0.80	143.481	150.197	109.550	150.228	107.011	150.197	114.970	150.086
0.85	143.453	150.172	109.538	150.195	107.022	150.170	114.929	150.095
0.90	143.425	150.142	109.534	150.155	107.042	150.140	114.900	150.099
0.95	143.413	150.114	109.561	150.118	107.083	150.112	114.888	150.100
1	143.438	150.100	109.650	150.100	107.167	150.100	114.902	150.100

Table VII. Coefficients A_k (Eq. (4)), Standard Deviation s (Eq.(8)), Durbin-Watson Statistic d , and $(V^E)_{x=0.5}$ and $\bar{V}_i^{E,\infty}$ at 25°C

System	A_0	A_1	A_2	A_3	A_4	$s \times 10^4$	d^a	$10^2(V^E)_{x=0.5}$ ($\text{cm}^3 \cdot \text{mol}^{-1}$)	$10^2 \bar{V}_1^{E,\infty}$ ($\text{cm}^3 \cdot \text{mol}^{-1}$)	$10^2 \bar{V}_2^{E,\infty}$ ($\text{cm}^3 \cdot \text{mol}^{-1}$)
1 + 2	0.024	0.0095	-0.0479	-0.024	0.101	4.85	2.62	0.60	9.20	6.31
1 + 3	0.264	-0.0046	-0.0646	0.481	0.120	6.04	2.60	6.60	27.60	36.31
1 + 4	0.250	0.0446	0.0244	-0.014	0.081	5.13	2.58	6.25	32.51	38.65
1 + 5	-0.777	0.0760	0.0354	0.095		7.59	2.16	-19.43	-91.25	-57.10

$$^a d = \sum_{u=2}^N (\epsilon_u - \epsilon_{u-1})^2 / \sum_{u=1}^N \epsilon_u^2; \epsilon_u = V_{u,\text{calc}}^E - V_{u,\text{expt}}^E.$$

Table VIII. Coefficients a_k (Eq. (5)), Standard Deviation s (Eq. (8)), Durbin-Watson Statistic d , and $(V^E)_{x=0.5}$ and $\bar{V}_i^{E,\infty}$ at 25°C

System	a_0	a_1	a_2	a_3	a_4	$s \times 10^4$	d^a	$10^2 (\bar{V}^E)_{x=0.5}$ ($\text{cm}^3 \cdot \text{mol}^{-1}$)	$10^2 \bar{V}_1^{E,\infty}$ ($\text{cm}^3 \cdot \text{mol}^{-1}$)	$10^2 \bar{V}_2^{E,\infty}$ ($\text{cm}^3 \cdot \text{mol}^{-1}$)
1 + 2	0.0285	-0.00487	0.02590	-0.00957	0.0231	5.00	2.62	0.60	9.196	6.307
1 + 3	0.2667	0.02427	0.02539	0.01926	0.0274	6.2	2.60	6.61	0.276	0.363
1 + 4	0.2743	0.03626	0.06283	-0.00555	0.0186	5.29	2.58	6.25	0.325	0.386
1 + 5	-0.7654	0.13284	0.02360	0.03789		7.81	2.16	-19.40	-0.912	-0.571

$$a_d = \sum_{i=2}^N (e_i - e_{i-1})^2 / \sum_{i=1}^N e_i^2, e_i = V_{i,\text{calc}}^E - V_{i,\text{expt}}^E.$$

to experimental errors, particularly in the dilute ranges and is helpful for detecting outliers. In addition, its values at infinite dilution represent the values of the partial excess volume at infinite dilution, $\bar{V}_i^{E,\infty}$, which can be also calculated from the adjustable parameters as follows [8]:

(a) *Redlich–Kister*

$$\bar{V}_1^{E,\infty} = A_0 - A_1 + A_2 - \dots = \bar{V}_1^\infty - V_1^0 \quad (9)$$

$$\bar{V}_2^{E,\infty} = A_0 + A_1 + A_2 + \dots = \bar{V}_2^\infty - V_2^0 \quad (10)$$

(b) *Legendre*

$$\bar{V}_1^{E,\infty} = a_0 - a_1 + a_2 - \dots = \bar{V}_1^\infty - V_1^0 \quad (11)$$

$$\bar{V}_2^{E,\infty} = a_0 + a_1 + a_2 + \dots = \bar{V}_2^\infty - V_2^0 \quad (12)$$

where V_i^0 is the molar volume of pure component i . The pertinent values of $\bar{V}_i^{E,\infty}$ are also shown in Tables VII and VIII. In addition, it should be realized that in the absence of homo-association, the value of the partial excess volume at infinite dilution reflects the true solute–solvent interaction. Equations (9) and (10) or (11) and (12) yield the same values of $\bar{V}_i^{E,\infty}$. Figure 2 shows a typical distribution of the residuals, which is random as shown by the Durbin–Watson statistic.

Inspection of the results of Tables II to V and Fig. 1 indicates that the excess volumes are positive for the binaries of 3-methylbutyl ethanoate (1) with butyl acrylate (2), ethyl acrylate (3), and methyl methacrylate (4), and negative for the binary with styrene (5). The magnitude and sign of V^E is a reflection of the type of interactions taking place in the mixture. This is very well exhibited by the mixtures studied here with the minimum and maximum values of V^E ranging from about -0.194 to $+0.066 \text{ cm}^3 \cdot \text{mol}^{-1}$. With regard to the symmetry of the excess function, Fig. 1 shows that the function $V^E(x)$ is essentially symmetric for all the systems, indicating that the maximum specific interaction occurs at about the equimolar composition.

As shown in Fig. 1, the mixture of 3-methylbutyl ethanoate and styrene presents a relative large contraction effect. This behavior may be the result of an inductive effect of the vinyl group in styrene, which enhances the electron density of its ring and the electrostatic interaction with the benzene ring, and of the vinyl group introducing a steric effect that operates in the opposite direction. The electron cloud of styrene interacts well with the ester group of the solvent and results in a contraction of the mixture. $n-\pi$ interactions between an aromatic hydrocarbon (such as styrene)

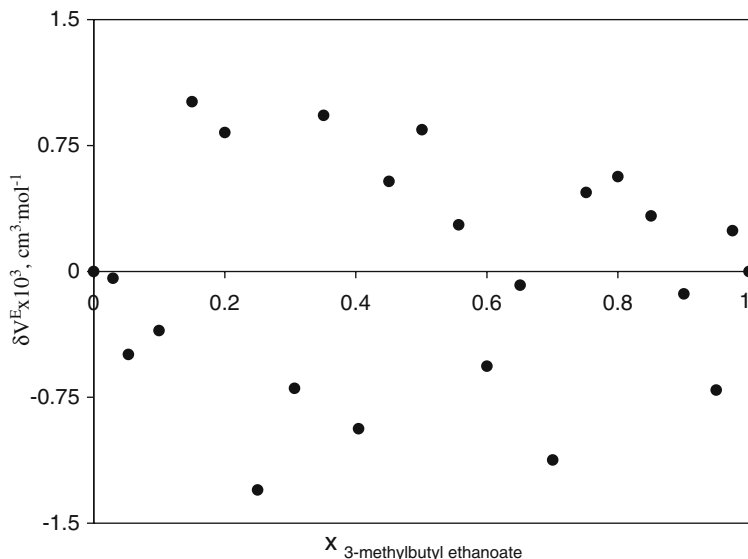


Fig. 2. Residual distribution plot for the 3-methylbutyl ethanoate + styrene system, according to the fit given in Table V.

and an ester are much stronger than those between a cyclic hydrocarbon (such as cyclohexane) and an ester. The negative sign indicates a net packing effect contributed by structural effects arising from interstitial accommodation.

The V^E curves are either positive or negative, the relative intensity depending on the nature of the solute (monomer) and the solvent. The overall positive magnitude of V^E for the systems with an acrylate monomer is the result of the breaking and dislocation of the ester's dipole-dipole association. In addition, the observed positive molar excess volumes point to their dependence with respect to the structure of the unsaturated ester: their values increase as the length of the ester chain decreases from ethyl to butyl, signaling a decrease of the contribution of interstitial accommodation and an increase of steric interference.

REFERENCES

1. R. D. Peralta, R. Infante, G. Cortez, L. Villarreal, and J. Wisniak, *Thermochim. Acta* **390**:47 (2002).
2. R. D. Peralta, R. Infante, G. Cortez, J. R. Torres-Lubián, and J. Wisniak, *Thermochim. Acta* **402**:247 (2003).

3. R. D. Peralta, R. Infante, G. Cortez, A. Cisneros, and J. Wisniak, *Thermochim. Acta* **398**:39 (2002).
4. R. D. Peralta, R. Infante, G. Cortez, O. Rodríguez, and J. Wisniak, *J. Solution Chem.* **31**:175 (2002).
5. R. D. Peralta, R. Infante, G. Cortez, R. G. López, and J. Wisniak, *Int. J. Thermophys.* **24**:173 (2003).
6. R. D. Peralta, R. Infante, G. Cortez, R. R. Ramírez, and J. Wisniak, *J. Chem. Thermodynamics*, **35**:239 (2003).
7. R. D. Peralta, R. Infante, G. Cortez, L. F. Ramos, and J. Wisniak, *Phys. Chem. Liq.* **41**:361 (2003).
8. H. C. Van Ness and M. M. Abbott, *Classical Thermodynamics of Nonelectrolyte Solutions* (McGraw-Hill, New York, 1982).
9. O. Redlich and A. T. Kister, *Ind. Eng. Chem.* **40**:345 (1948)
10. J. Tomiska, *CALPHAD* **5**:93 (1981).
11. J. Tomiska, *CALPHAD* **8**:283 (1984).
12. J. Wisniak and A. Polishuk, *Fluid Phase Equilib.* **164**:61 (1999).
13. S. A. Karpushina, M. T. Khimenko, and Yu. N. Surov, *Zh. Fiz. Khim.* **64**:368 (1990).
14. N. V. Sastry and M. K. Valand, *Phys. Chem. Liq.* **3**: 61 (2000).
15. L. Beichen, S. E. M. Hamam, and B. C.-Y Lu, *J. Chem. Thermodyn.* **18**:1043 (1986)
16. *TRC Thermodynamic Tables, extant 2002. Hydrocarbons*, Thermodynamics Research Center, The Texas A&M University System, College Station, Texas; table a-4490, styrene (1989).